

科目名稱	材料力學	類組代碼	D37
		科目碼	D3793

※本項考試依簡章規定所有考科均「不可」使用計算機。 本科試題共計 3 頁

全部單選題，每題 10 分，答錯不倒扣。

- A simply supported beam is loaded through the attached bracket BDE, as shown in Fig. 1. The reaction force at support C is:

(A) $3P/7$ (B) $4P/7$ (C) $5P/7$ (D) $6P/7$ (E) None of the above

Fig.1
- Continuing from Problem 1, the magnitude of the maximum bending moment in beam ABC is:

(A) $4PL/21$ (B) $5PL/21$ (C) $5PL/12$ (D) $5PL/14$ (E) None of the above
- A nonprismatic bar has an internal cylindrical hole of diameter $d/2$ in Segment 1 (see Fig. 2). Assume that Young's modulus E is constant. For the loadings shown in Fig.2, the internal axial forces N_1 and N_2 in Segment 1 and Segment 2 are:

(A) $N_1 = P/2$ and $N_2 = P/2$ (B) $N_1 = P/2$ and $N_2 = -P/2$
 (C) $N_1 = -P/2$ and $N_2 = P/2$ (D) $N_1 = 3P/2$ and $N_2 = -P/2$ (E) None of the above

Fig. 2
- Continuing from Problem 3, if the axial displacement at end 3 is $4PL/E(\pi d^2)$, the length of the hollow segment is:

(A) $x = 3L/7$ (B) $x = 4L/7$ (C) $x = 6L/7$ (D) $x = 9L/7$ (E) None of the above
- A prismatic bar AB of length L , cross-sectional area A , Young's modulus E , and total weight W hangs vertically under its own weight, as shown in Fig. 3. The elongation of the entire bar is:

(A) $2WL/EA$ (B) $WL/2EA$ (C) WL/EA (D) $WL/4EA$ (E) None of the above

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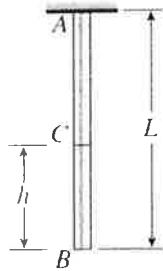


Fig. 3

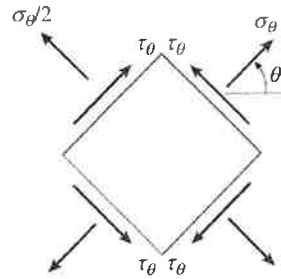


Fig. 4

6. Continuing from Problem 5, the internal axial force at section C, located a distance h from end B, is:
- (A) $N = WL/h$ (B) $N = Wh/L$ (C) $N = W(L - h)/h$ (D) $N = W(L - h)/L$
 (E) None of the above

7. A plane stress element in a bar subjected to uniaxial stress (at $\theta = 0^\circ$) is shown in Fig. 4. The shear stress τ_θ and maximum shear stress τ_{max} are :

- (A) $\tau_\theta = -\frac{1}{\sqrt{2}}\sigma_\theta$ and $\tau_{max} = \frac{3}{4}\sigma_\theta$ (B) $\tau_\theta = \frac{1}{\sqrt{2}}\sigma_\theta$ and $\tau_{max} = \frac{3}{2}\sigma_\theta$
 (C) $\tau_\theta = -\frac{1}{2\sqrt{2}}\sigma_\theta$ and $\tau_{max} = \frac{3}{4}\sigma_\theta$ (D) $\tau_\theta = \frac{1}{2\sqrt{2}}\sigma_\theta$ and $\tau_{max} = \frac{3}{2}\sigma_\theta$
 (E) None of the above

8. A composite bar is made of two different metals with Young's moduli E_1 and E_2 , as shown in Fig. 5. The two parts of the bar have the same cross-sectional dimensions. The bar is compressed by forces P acting through rigid end plates. The line of action of the forces P has an eccentricity e . If each part of the bar is uniformly stressed in compression, the eccentricity e is :

- (A) $e = \frac{b(E_2 - E_1)}{(E_1 + E_2)}$ (B) $e = \frac{b(E_2 + E_1)}{(E_1 - E_2)}$ (C) $e = \frac{b(E_2 - E_1)}{2(E_1 + E_2)}$ (D) $e = \frac{b(E_2 + E_1)}{2(E_1 - E_2)}$
 (E) None of the above

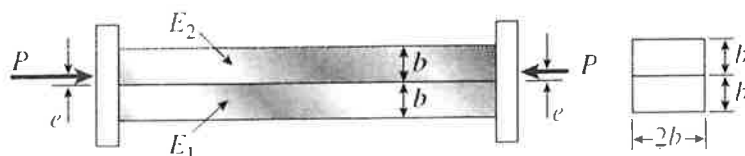


Fig. 5

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9. For beam AB, with flexural rigidity EI and section modulus S , carrying a triangularly distributed load of maximum intensity q_0 , as shown in Fig.6, the maximum tensile stress in beam AB is :

- (A) $\frac{q_0 L^2}{3\sqrt{3}S}$ (B) $\frac{q_0 L^2}{6\sqrt{3}S}$ (C) $\frac{q_0 L^2}{9\sqrt{3}S}$ (D) $\frac{q_0 L^2}{9S}$ (E) None of the above

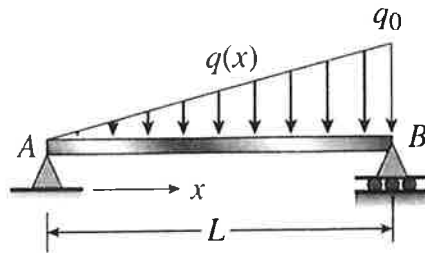


Fig. 6

10. Continuing from Problem 9, the deflection $v(x)$ is:

- (A) $v(x) = \frac{q_0}{360LEI} (3x^5 + 20L^2x^3 - 15x^4L)$
 (B) $v(x) = \frac{q_0}{120LEI} (x^5 - 5Lx^4 + 10L^2x^3 - 10L^3x^2)$
 (C) $v(x) = \frac{q_0}{120LEI} (x^5 - 5Lx^4 + 20L^2x^3 - 16L^5)$
 (D) $v(x) = \frac{q_0}{360LEI} (-3x^5 + 10L^2x^3 - 7L^4x)$
 (E) None of the above